[3 Hours]

[Total Marks: 80]

[05]

# Instructions to the candidates if any:-

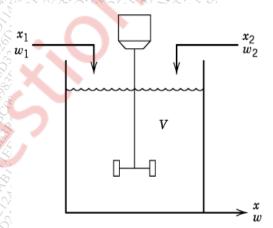
- 1. Question No 1 is compulsory
- 2. Attempt any three questions from the remaining five questions
- 3. Assume suitable data wherever necessary
- 4. Figures to the right indicates full marks

#### Q. No. 1

- a. Discuss the following with an example
  - Disturbance variable
  - ii. Controlled variable
  - iii. Manipulated variable
- b. Derive the transfer function for a parallel form of PID controller. [05]
- c. Explain why mercury in glass thermometer is a first order system. [05]
- d. Write a short note on Nyquist stability criterion. [05]

## Q. No. 2

a. Derive the dynamic model for the isothermal blending process which is shown in the following figure.



 $w_1$ ,  $w_2$  and w are the mass flow rates.

 $x_1$ ,  $x_2$  and x are the mass fraction of component A in  $w_1$ ,  $w_2$  and w respectively.

V is the volume of the liquid in the tank.

[10]

b. A composition sensor is used to continuously monitor the contaminant level in a liquid stream. The transfer function of the sensor is given as-

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$$\frac{C_m(s)}{C(s)} = \frac{1}{17s+1}$$

Where C is the deviation in the actual concentration and  $C_m$  is the deviation in the measured value. The process is at steady state initially, with the contamination at 6 ppm, when the input starts increasing as c(t) = 5 + 0.3t, where t is in sec. an alarm sounds if the measured value exceeds the environmental limit of 9 ppm. Both c and  $c_m$  are 6 ppm at initial steady state. After the actual concentration exceeds the limit, how long will it take for the alarm to sound?

#### Q. No. 3

a. The model of the electrically heated stirred-tank system is given by the following equations

$$\frac{dT}{dt} = \frac{w}{\rho V} (T_i - T) + \frac{h_E A_E}{\rho V C_P} (T_E - T)$$

$$\frac{dT_E}{dt} = \frac{Q}{m_E C_{PE}} - \frac{h_E A_E}{m_E C_{PE}} (T_E - T)$$

- i. Derive transfer functions relating changes in outlet temperatures T to changes in two input variables: the heater input Q and inlet temperature  $T_i$ .
- ii. Show how these transfer functions are simplified when negligible thermal capacitance of the heating element is assumed. [10]
- b. With usual notations, derive the closed loop transfer function for a servo problem [10]

## Q. No. 4

a. A single tank process has been operating for a long period of time with the inlet flow rate  $q_i$  equal to 30.4 lit/min. After the operator increase the flow rate suddenly at t = 0, by 16 %, the change in the liquid level in the tank occurs as shown in the following table.

t (min)	0000	0.2	0.4	0.6	0.8	1.0	1.2
□ (cm)	5.50	<sup>y</sup> 5.75	5.93	6.07	6.18	6.26	6.32
t (min)	1.4	1.6	1.8	2.0	3.0	4.0	5.0
□ (cm)	6.37	6.40	6.43	6.45	6.50	6.51	6.52

Assume that the process dynamics can be described by a first order model. Calculate the steady state gain and the time constant by using

- i. From the time required for the output to reach 63.2 % of the total change.
- ii. From the slope of the fraction incomplete response curve.

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iii. From the initial slope of the response curve.

[15]

b. Discuss the characteristic of a control valve. [05]

## Q. No. 5

- a. Discuss general stability criterion for stability of a closed loop system. [10]
- b. Consider a feedback control system in which  $G_C(s) = K_C$ ,  $G_V(s) = \frac{1}{5s+1}$ ,  $G_P(s) = G_d(s) = \frac{1}{5s+1}$  and  $G_m(s) = 1$ . Determine the range of  $K_C$  for which the system is closed loop stable.

# Q. No. 6

- a. Discuss frequency response of a second order system. [10]
- b. Consider the following T.F. Of a first order processes with dead time

$$G_P(s) = \frac{2e^{-0.5s}}{(\tau s + 1)}$$

A proportional controller is used to complete negative feedback loop with the process. When the controller gain is set equal to 2.5, the phase margin is found to be 30°. What is the value of process time constant? What is the corresponding gain margin? [10]



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